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**AMENDMENTS IN THE CLAIMS:**

1. (Currently Amended) A power control circuitry for controlling the output power level ( $P_{out}$ ) of a signal ( $x(t)$ ) to be transmitted at the output port of a variable-gain power amplifier (105), said power control circuitry (101M+N) comprising a current sense loop (101M) with an integrated comparator stage (112'') having a first input port supplied with a reference signal ( $V_{ref}$ ) representing the nominal power level ( $P_{ref}$ ) for the output power ( $P_{out}$ ) and a second input port supplied with a signal from a current sensor (204) which is placed in the power supply line of a variable-gain power amplifier (105), wherein the output signal of said comparator stage (112'') is fed to the power control input port of the variable-gain power amplifier (105),

characterized by and further comprising

- power sensing means (108) for detecting the power of a feedback signal ( $V_{PD}$ ) representing the reflected wave of the signal ( $x(t)$ ) to be transmitted, and
- a feedback loop (101N) for feeding said reference signal ( $V_{ref}$ ) derived from said feedback signal ( $V_{PD}$ ) and a reference ramp signal ( $V_{ramp}$ ) to the first input port of the comparator stage (112'') in order to increase the radiated power ( $P_{out}$ ) of said signal ( $x(t)$ ) in case a transmit antenna (110) is mismatched to the variable-gain power amplifier (105).

2. (Currently Amended) A power control circuitry according to claim 1,

characterized by including

signal processing means comprising

- a multiplier (301b) for multiplying a processed version ( $K \cdot G_{OP} \cdot V_{PD}$ ) of the feedback signal ( $V_{PD}$ ) by the reference ramp signal ( $V_{ramp}$ ),
- a summation element (301a), used for adding the output signal ( $V_{ramp} \cdot K \cdot G_{OP} \cdot V_{PD}$ ) of the multiplier (301b) to the reference ramp signal ( $V_{ramp}$ ), thereby yielding said reference signal ( $V_{ref}$ ).

3. (Currently Amended) A power control circuitry according to claim 1,

characterized by including

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digital signal processing means ~~(201C)~~ comprising a multiplication element ~~(301b')~~ for multiplying a gain factor ( $\chi := 1 + K \cdot G_{OP} \cdot V_{PD}$ ) supplied by a gain factor control unit ~~(301e)~~ by the reference ramp signal ( $V_{ramp}$ ), wherein  $K$  is a normalization factor (in  $V^{-1}$ ) and  $G_{OP}$  denotes the gain factor of an operational amplifier ~~(303)~~ in said feedback loop ~~(101N)~~, thereby yielding said reference signal ( $V_{ref}$ ).

4. (Currently Amended) A power control circuitry according to ~~anyone of the claims 1 to 3~~ claim 1,

~~characterized by including~~

decoupling means ~~(106)~~ at the output port of the variable-gain power amplifier ~~(105)~~ for providing a feedback signal ( $V_{PD}$ ).

5. (Currently Amended) A power control circuitry according to claim 4,

~~characterized in that~~ wherein

said decoupling means ~~(106)~~ is realized as a directional coupler ~~(106')~~ or a circulator ~~(106'')~~.

6. (Currently Amended) A method for stabilizing the power level ( $P_{out}$ ) of a signal ( $x(t)$ ) to be transmitted at the output port of a variable-gain power amplifier ~~(105)~~,

said method being characterized by the following steps:

- detecting ~~(S1)~~ the voltage level ( $V_{PD}$ ) of a feedback signal which represents the reflected wave of said signal ( $x(t)$ ),
- calculating ~~(S1A)~~ a reference signal ( $V_{ref}$ ) representing the nominal power level ( $P_{ref}$ ) for the output power ( $P_{out}$ ) of the RF output signal ( $x(t)$ ) as a function of a reference ramp signal ( $V_{ramp}$ ) and said feedback signal ( $V_{PD}$ ),
- feeding ~~(S2)~~ the obtained reference signal ( $V_{ref}$ ) to a first input port of a comparator stage ~~(112')~~ in the feedback chain of the current sense loop ~~(101M)~~,
- feeding ~~(S4)~~ a signal representing the DC supply current ( $I_{PA}$ ) of the variable-gain power amplifier ~~(105)~~ to a second input port of said comparator stage ~~(112')~~,
- comparing ~~(S5)~~ the voltage level of the signal derived from said voltage drop ( $U_{RM}$ ) with the voltage level of said reference signal ( $V_{ref}$ ),
- feeding ~~(S6)~~ a signal being a function of the difference between the signal derived from

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said voltage drop ( $U_{RM}$ ) and the calculated reference signal ( $V_{ref}$ ) to a first input port of the power amplifier (105), and

- adjusting (S7) the current power level ( $P_{out}$ ) by amplifying the difference between the output signal of said comparator stage (112') and the signal ( $x(t)$ ) to be transmitted before being amplified at a second input port of the variable-gain power amplifier (105).

7. (Currently Amended) A method according to claim 6,

~~characterized in that~~ wherein

the step (S1A) of calculating said reference signal ( $V_{ref}$ ) comprises the following steps:

- multiplying (S1a') a processed version ( $K \cdot G_{OP} \cdot V_{PD}$ ) of the feedback signal ( $V_{PD}$ ) by the reference ramp signal ( $V_{ramp}$ ) and
- adding (S1a'') the output signal ( $V_{ramp} \cdot K \cdot G_{OP} \cdot V_{PD}$ ) of the multiplication step (S1a') to the reference ramp signal ( $V_{ramp}$ ), thereby yielding said reference signal ( $V_{ref}$ ).

8. (Currently Amended) A method according to claim 6,

~~characterized in that~~ wherein

the step (S1A) of calculating said reference signal ( $V_{ref}$ ) comprises the step of multiplying (S1b) a gain factor ( $\chi := 1 + K \cdot G_{OP} \cdot V_{PD}$ ), which is supplied by a gain factor control unit (301e), by the reference ramp signal ( $V_{ramp}$ ), thereby yielding said reference signal ( $V_{ref}$ ).

9. (Currently Amended) A wireless telecommunication device,

~~characterized by~~ including

a mobile RF transmitter (300a, 300b or 300e) comprising a power control circuitry (101M+N) according to ~~anyone of the claims 1 to 5~~ claim 1.